Carissa Farkas Structural Engineering, PLLC 206.683.3197

Supplemental Structural Calculations for: 61st St SE MI

Project Address: 3038 61st St SE Mercer Island, WA 98040

Design per 2018 International Building Code



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RetainPro (c) 1987-2018, Build 11.18.12.04 License : KW-06064278 License To : cfse			Cantilevered Retaining Wall			Code: IBC 2015,A	CI 318-14,ACI 530-13	
Criteria				Soil Data				
Retained Height Wall height above soil Slope Behind Wall	= = =	7.00 ft 0.00 ft 0.00	/ E /	Allow Soil Bearing = Equivalent Fluid Pressure Meth Active Heel Pressure =	2,000.0 nod 35.0	psf psf/ft		
Height of Soil over Toe Water height over heel	=	6.00 in 0.0 ft	F S F S	= Passive Pressure = Soil Density, Heel = Soil Density, Toe = Footing Soil Friction = Soil height to ignore for passive pressure =	350.0 120.00 0.00 0.450 12.00	psf/ft pcf pcf in		
Surcharge Loads				Lateral Load Applied to	o Stem		Adjacent Footing I	oad
Surcharge Over Heel Used To Resist Slidin Surcharge Over Toe Used for Sliding & Ove Axial Load Applie Axial Dead Load Axial Live Load Axial Load Eccentricity	g & Ov = erturnir d to ; = = =	0.0 psf rerturning 0.0 ng Stem 0.0 lbs 0.0 lbs 0.0 in		Lateral Load = Height to Top = Height to Bottom = Load Type = W (S Wind on Exposed Stem = (Service Level)	0.0 #/ 0.00 ft 0.00 ft /ind (W) Service Le 0.0 pt	/ft evel) sf	Adjacent Footing Load Footing Width Eccentricity Wall to Ftg CL Dist Footing Type Base Above/Below Soil at Back of Wall Poisson's Ratio	= 0.0 lbs = 0.00 ft = 0.00 in = 0.00 ft Line Load = 0.0 ft = 0.300
Earth Pressure S Method : Uniform Multiplier Used (Multiplier used on soil	eism = densit	7.000 7)		Uniform Seismic Force = Total Seismic Force = 4	54.833 29.528			
Design Summary				Stem Construction		Bottom		
Wall Stability Ratios				Design Height Above F	tg ft =	0.00		
Sliding	=	3.18 OK 1.50 OK		Wall Material Above "H Design Method Thickness	lt" = = =	Concrete LRFD 8.00		
Total Bearing Loadresultant ecc.	= =	4,289 lbs 6.73 in		Rebar Size Rebar Spacing	= =	# 5 8.00		
Soil Pressure @ Toe Soil Pressure @ Heel	= =	1,370 psf 290 psf	OK OK	fb/FB + fa/Fa	=	0.384	· •	
Soil Pressure Less	= 5 Than	Allowable		Total Force @ Sectio	n Ibc –			
ACI Factored @ Toe ACI Factored @ Heel	=	1,917 psf 406 psf	014	Strength Level MomentActual	lbs =	1,755.8		
Footing Shear @ Heel Allowable	= = =	9.4 psi 75.0 psi	OK OK	Service Level Strength Level	ft-# = ft-# =	4,544.8	3	
Sliding Calcs Lateral Sliding Force less 100% Passive Forc	= e = -	1,374.5 lbs 136.1 lbs		MomentAllowable ShearActual Service Level	= psi =	11,799.2		
Added Force Req'd Added Torce Req'd for 1.5 Stability	e = - = =	1,930.1 lbs 0.0 lbs 0.0 lbs	ok ok	Strength Level ShearAllowable Anet (Masonry) Rebar Depth 'd'	psi = psi = in2 = in =	23.6 75.0 6.19		
				Masonry Data f'm Fs Solid Grouting	psi = psi = =			
Vertical component of act NOT considered in the ca	ive late Iculatio	eral soil press on of soil bear	ure IS ing	Modular Ratio 'n' Wall Weight	= psf =	100.0		
Load Factors ———— Building Code	IE	3C 2015,ACI		 Short Term Factor Equiv. Solid Thick. 	=			

Masonry Block Type

Concrete Data

f'c

Fy

Masonry Design Method

= Medium Weight

2,500.0

= ASD

psi = 60,000.0

psi =

Loud i dotoi o	
Building Code	IBC 2015,ACI
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.000
Seismic, E	1.000

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Concrete Stem Rebar Area De	tails					
Bottom Stem	Vertical Reinforcing	Horizontal Reinforci	ng			
As (based on applied moment) :	0.1721 in2/ft					
(4/3) * As :	0.2295 in2/ft	Min Stem T&S Rein	Min Stem T&S Reinf Area 1.344 in2			
200bd/fy : 200(12)(6.1875)/60000 :	0.2475 in2/ft	Min Stem T&S Rein	Min Stem T&S Reinf Area per ft of stem Height : 0.192 in2/ft			
0.0018bh : 0.0018(12)(8) :	0.1728 in2/ft	Horizontal Reinforci	Horizontal Reinforcing Options :			
		One layer of : T	wo layers of :			
Required Area :	0.2295 in2/ft	#4@ 12.50 in	#4@ 25.00 in			
Provided Area :	0.465 in2/ft	#5@ 19.38 in	#5@ 38.75 in			
Maximum Area :	0.8382 in2/ft	#6@ 27.50 in	#6@ 55.00 in			
Footing Dimensions & Stren	gths Footing	g Design Results				
Toe Width=1Heel Width= $\frac{4}{5}$ Footing Thickness=Footing Thickness=10Key Width=0Key Depth=0Key Distance from Toe=0f'c =2,500 psiFy =60,cFooting Concrete Density=150Min. As %=0.00Cover @ Top2.00@ Btm.=	.00 ft .17 Factored Product .17 Mu': Upward .00 in Mu': Downwe .00 in Mu': Design .00 in Actual 1-Way .00 in Allow 1-Way .00 ft Toe Reinford .00 psi Heel Reinford .00 pcf Key Reinford .18 Other Accee 3.00 in Toe: Not Heel: #40 Key: No Min footin If one lays #4@ 11 #5@ 17 #6@ 24 #6@ 24	Toeessure= $1,917$ d= 910 vard= 111 = 799 vy Shear= 7.66 / Shear= 40.00 cing=None Spec'dcing=# 4 @ 9.99 incing=None Spec'dptable Sizes & Spacingscreq'd: Mu < phi*5*lambda*s	Heel 406 psf 4,584 ft-# 7,106 ft-# 2,522 ft-# 9.35 psi 75.00 psi Seqrt(f'c)*Sm 6@ 24.43 in, #7@ 33.32 in, #8@ 43.88 in, #9@ 5 1.12 in2 0.22 in2 /ft If two layers of horizontal bars: #4@ 22.22 in #5@ 34.44 in #6@ 48.89 in			

Summary of Overturning & Resisting Forces & Moments

		OV	ERTURNING	.
Item		Force lbs	Distance ft	Moment ft-#
Heel Active Pressure	=	1,073.8	2.61	2,803.9
Surcharge over Heel	=			
Surcharge Over Toe	=			
Adjacent Footing Load	=			
Added Lateral Load	=			
Load @ Stem Above So	il =			
Seismic Earth Load	=	300.7	3.92	1,177.6
	=			
Total		1,374.5	О.Т.М.	3,981.5
	=		=	
Resisting/Overturning	g Ra	tio	=	3.18
Vertical Loads used for	or So	il Pressure	= 4,289	1 lbs

		Force lbs	Distance ft	ft-#
Soil Over Heel	=	2,942.8	3.42	10,059.5
Sloped Soil Over Hee	=			
Surcharge Over Heel	=			
Adjacent Footing Load	= t			
Axial Dead Load on S	tem =			
* Axial Live Load on Ste	em =			
Soil Over Toe	=		0.50	
Surcharge Over Toe	=			
Stem Weight(s)	=	700.0	1.33	933.3
Earth @ Stem Transit	ions =			
Footing Weight	=	646.3	2.59	1,670.6
Key Weight	=			
Vert. Component	=			
Т	otal =	4,289.1	lbs R.M.=	12,663.4

.....RESISTING.....

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

If seismic is included, the OTM and sliding ratios be 1.1 per section 1807.2.3 of IBC 2009 or IBC 201

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

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Tilt			
Horizontal Deflection at Top of Wa	II due to settlen	nent of soil	
(Deflection due to wall bending not considered	(t		
Soil Spring Reaction Modulus	250.0	рсі	
Horizontal Defl @ Top of Wall (approximate or	nly) 0.052	in	
The above calculation is not valid if the heel so	oil bearing pressure	exceeds that of the toe,	
because the wall would then tend to rotate into	o the retained soil.		